



# Combustion/Pyrolysis of Oil Palm Stones and Palm Kernel Cake



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## Introduction/Main Objective

Biomass is important for new energy sources because it is an indigenous, considerably cheap and, above all, renewable fuel. By-products or waste from the palm oil mills are generated in significant amounts and mainly consists of Empty Fruit Bunches (EFB), Oil Palm Stones (OPS), Oil Palm Shell (OPSh), Palm Kernel Cake (PKC) and Palm Oil Mill Effluent (POME). These waste are currently not fully utilised as a fuel. Pelletisation of PKC is very important in order to utilise it as a fuel. The loose PKC raw material need to be densified and form a homogeneous product before it can be burnt.

The main objective of this PhD study is to investigate the main characteristics of the thermo-chemical conversion of OPS and PKC. A series of combustion and pyrolysis tests were carried out by using OPS and PKC as the raw materials in two fixed bed reactors. In addition, the FLIC code was used to predict the key parameters, such as for theoretical solid temperature and gas composition. These parameters were used to validate the experimental results. The main parameter investigated in the combustion tests was the effect of air flow rates on the thermal characteristics of OPS material.

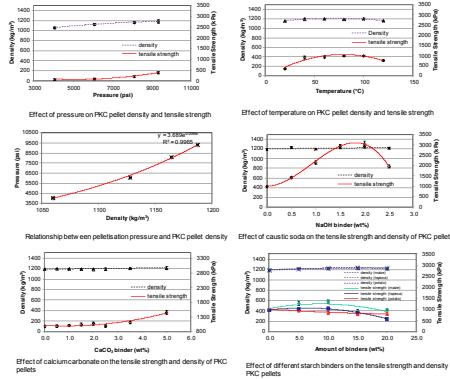
## Experimental Programmes



Pelletiser

### Experimental conditions

Properties	Test conditions
Moisture (%)	1.9, 7.9, 9
Pressure (MPa)	27.04, 24.47, 41.37, 44.29, 55.16, 52.03
Temperature (°C)	20, 40, 60, 80, 100, 120
Binders	4%
Caustic soda	0.5, 1.0, 1.5, 2.0, 2.5
Carbonate	0.5, 1.0, 1.5, 2.0, 2.5, 3.0, 3.5
Melax extract	0.5, 1.0, 1.5, 2.0
Tapach water	0.5, 1.0, 1.5, 2.0
Polystyrene	0.5, 1.0, 1.5, 2.0



The optimum conditions for the production of PKC pellets were found at moisture content of 7.9 % (gas received), pressure of 64.38 MPa and temperature of 80-100 °C.

Small additions of caustic soda improved quality of PKC pellets in terms of tensile strength and density by 61% and 20% respectively.

Pellet produced at different moisture contents: (a) 19%, (b) 7.9%, and (c) 9%

## Combustion and Pyrolysis Tests: Results and Discussion



Fixed Bed Reactor (Pilot Burner)

**Combustion:** The combustion tests were conducted in a counter-current feed-bed reactor.  
 Reactor: interior tube: Inconel 600 nickel alloy tube (8 mm thickness)  
 Dimensions of the reactor: ID: 200 mm, H: 1500 mm  
 Maximum temperature: 1250 °C  
 The grate was a stainless steel perforated plate with approximately 700 holes of 2 mm in diameter.



Fixed Bed Pyrolyser

**Pyrolysis:** The pyrolyser unit consists of: Two furnaces, Temperature controller, condenser.  
 Reactors: Made from 316 stainless steel.  
 Dimensions: ID: 125 mm, H: 300 mm  
 Maximum temperature: 1000 °C.  
 Gas outlet hole of 36 mm at the top of the reactor.

Material	Case	Combustion parameters			
		Weight (kg)	Bed Height (mm)	Air Flow-Rate (l/min)	Equivalent Ratio (λ)
OPS	001	6.00	320	0.33	3.0
	002	6.00	320	400	0.60
	003	4.12	220	600	0.80
	004	6.00	320	800	0.87

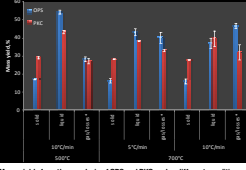
Material	Weight (g)	Operating conditions for pyrolysis tests		
		Set Temp. (°C)	Heating Rate (°C/min)	A <sub>0</sub> flow rate (l/min)
OPS	200	500 and 700	5, 10 and 15	1.5
PKC	200	500 and 700	5, 10 and 15	1.5

## Raw Materials



Proximate and ultimate analysis of OPS and PKC samples											
	Proximate analysis (% as received)					Ultimate analysis (% dry)					
	M	VM	FC	Ash	C	H	O	N	S	Cl	
OPS	4.71	66.00	6.50	2.24	72.94	0.11	16.24	1.70	0.37	200	27.46
PKC	7.52	71.84	16.48	59.81	6.43	30.45	3.25	0.33	380	18.87	

## Results from pyrolysis tests



The char yields obtained from the OPS were lower compared to those produced from the PKC, but the gas yields from the OPS were higher.

All char samples mainly consists of fixed carbon (FC).

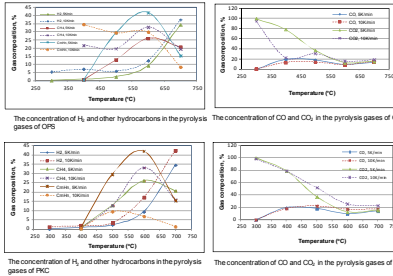
The calorific value (HHV) were approximately 28 MJ/kg (energy content as high as bituminous coal).

liquid derived from OPS formed a homogeneous mixture, while the liquid obtained from PKC consists of two distinct liquids.

The calorific values of the liquid ranges from 21 to 38 MJ/kg.

Proportion of reactor sample from pyrolysis of the OPS and PKC										
Proximate analysis (% as received)	OPS char					PKC char				
	Moisture	VM	FC	Ash	C	Moisture	VM	FC	Ash	C
Moisture	1.14 ± 0.24	1.18 ± 0.12			51.17 ± 0.11	1.14 ± 0.24	1.18 ± 0.12			51.17 ± 0.11
Ash	10.23 ± 1.96	13.10 ± 0.29			14.42 ± 0.16	10.23 ± 1.96	13.10 ± 0.29			14.42 ± 0.16
VM	14.05 ± 0.24	6.4 ± 0.23			12.49 ± 0.26	14.05 ± 0.24	6.4 ± 0.23			12.49 ± 0.26
FC	68.48	79.31			75.18	68.48	79.31			75.18
Ultimate analysis (% dry)										
C	80.27 ± 2.70	84.56 ± 2.29			62.76 ± 1.67	80.27 ± 2.70	84.56 ± 2.29			62.76 ± 1.67
H	2.11 ± 0.40	1.33 ± 0.40			3.12 ± 0.31	2.11 ± 0.40	1.33 ± 0.40			3.12 ± 0.31
O	13.15	10.17			20.05	13.15	10.17			20.05
N	4.42 ± 0.20	3.73 ± 0.40			4.29 ± 0.11	4.42 ± 0.20	3.73 ± 0.40			4.29 ± 0.11
S	0.04 ± 0.01	0.14 ± 0.15			0.02 ± 0.02	0.04 ± 0.01	0.14 ± 0.15			0.02 ± 0.02
Gross calorific value (MJ/kg)	27.8 ± 1.1	28.3 ± 0.40			28.1 ± 0.2	27.8 ± 1.1	28.3 ± 0.40			28.1 ± 0.2

Proportion of multiple products from pyrolysis of the OPS and PKC										
CV (MJ/kg)	OPS					PKC (at 800 °C)				
	500 °C	700 °C	500 °C	700 °C	900 °C	500 °C	700 °C	500 °C	700 °C	900 °C
Moisture	64.47	9.9			1.5	64.47	9.9			1.5
VM	10.53	10.54			10.53	10.53	10.54			10.53
Hydrogen	3.23	4.50			4.50	3.23	4.50			4.50
Nitrogen	1.05	1.67			1.67	1.05	1.67			1.67
Sulphur	0.23	0.41			0.41	0.23	0.41			0.41
Empirical formula	CH <sub>1.41</sub> O <sub>1.1</sub>	CH <sub>1.41</sub> O <sub>1.1</sub>			CH <sub>1.41</sub> O <sub>1.1</sub>	CH <sub>1.41</sub> O <sub>1.1</sub>	CH <sub>1.41</sub> O <sub>1.1</sub>			CH <sub>1.41</sub> O <sub>1.1</sub>



The gas consists mainly of CO<sub>2</sub>, CO, H<sub>2</sub>, CH<sub>4</sub> and other hydrocarbons.

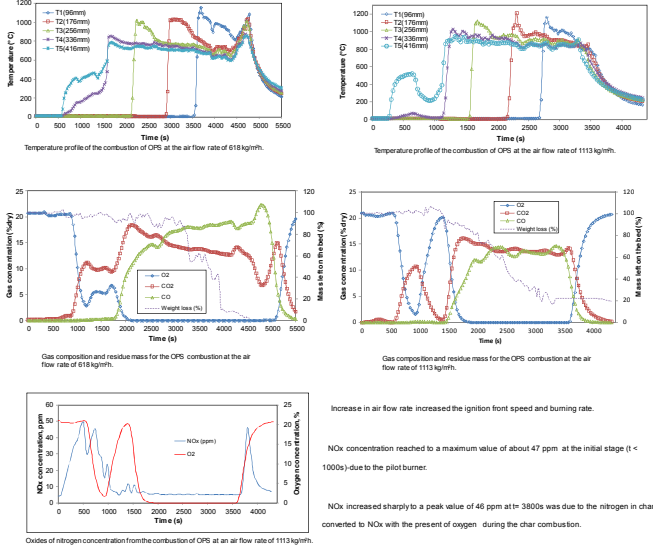
CO<sub>2</sub> and CO were mainly evolved at low temperatures (< 500 °C).

At high temperature (> 500 °C) H<sub>2</sub> and other hydrocarbons (C<sub>2</sub>-C<sub>4</sub>) were the dominant component in the gas products.

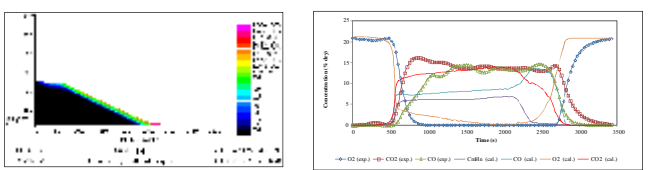
Most of the light HC gases start to evolve at temperature > 300 °C.

The maximum H<sub>2</sub> concentration 35-45% was reached at the temperature of 700 °C.

## Results from combustion tests



## Results from FLIC simulation



The predicted temperature profile during the ignition propagation stage was almost similar to the experimental results.

At this stage, the temperature increased to a maximum of 1400 K.

At approximately t = 2400-2500s, the ignition front reached the bottom of the bed.

In general, the predicted gas composition was in good agreement with the measured data.

Some minor discrepancies including the predicted concentrations of CO<sub>2</sub> and CO were slightly lower than the measured data.

## Conclusions

The optimum conditions for the production of PKC pellets were found to be a moisture content of 7.9%, pressure 62.05 MPa and temperature 80 - 100 °C.

Pyrolysis of the OPS and PKC at 700 °C with a heating rate of 10 °C/min gave maximum liquid yield of 57.92 and 42.84 wt% respectively.

The pyrolysis gases consists mainly of CO and CO<sub>2</sub>, and evolved at lower temperature, below 500 °C.

The main gases that evolved at the high temperature region (> 500 °C) were hydrogen and other hydrocarbons gases (C<sub>2</sub>-C<sub>4</sub>).

The results of the combustion tests showed that an increase in air flow rate increased the ignition front speed and burning rate.

The FLIC modelling results were in good agreement with the experimental results.

## Future work

The use of the binders should be investigated further in order to produce good quality of PKC pellets.

In order to compare the combustion characteristics between two different combustion systems, further experimental study is necessary to be carried out by using fluidised bed reactor.

Further investigation must be done on a broad range of combustion air flow rates for better understanding towards the combustion behaviour of the OPS and PKC materials.

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